

Mathematische Analyse von FEM für Probleme in der Mechanik

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Boundary layers in thin structures

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Plan

- A Lamé boundary value problem in thin plates.
- A **two-scale** membrane or bending asymptotics for the displacement in thin plates.
- A **three-scale** asymptotics for the displacement in thin elliptic shells.
- A **numerical evidence** of the boundary layer for strains in a bending plate.
- Prospects.

Connection with literature, concerning theoretical aspects

- **Philippe CIARLET** and his group, concerning the **limits** as the thickness goes to 0.
- **Sergei NAZAROV** with co-authors and students, concerning asymptotics using refined **Korn inequalities** (in general requires clamped conditions).
- **Doug ARNOLD** with co-authors and students, concerning the asymptotics of the **2D models**, e.g. the Reissner-Mindlin model.

Three-Dimensional Equations in Linearly Elastic Plates

- **Displacement Field** $u = (u_1, u_2, u_3)$
- **Linearized Strain Tensor** $e = (e_{ij})_{1 \leq i, j \leq 3} : e_{ij}(u) = \frac{1}{2}(\partial_i u_j + \partial_j u_i)$.
- **Stress Tensor** $\sigma = (\sigma_{ij})_{1 \leq i, j \leq 3} : \sigma = A e$ (Hooke's law)
- **Matrix of Rigidity** of the constitutive material $A = (A_{ijkl}) : \text{symmetries}$

$$A_{ijkl} = A_{jikl} = A_{ijlk} = A_{klij}$$

Here we consider the simplest situation

Isotropic $A_{ijkl} = \lambda \delta_{ij} \delta_{kl} + \mu (\delta_{ik} \delta_{jl} + \delta_{il} \delta_{jk})$ with Lamé coeff. λ and μ

- **Volumic Force Field** $f = (f_1, f_2, f_3)$ (Equations of Equilibrium)

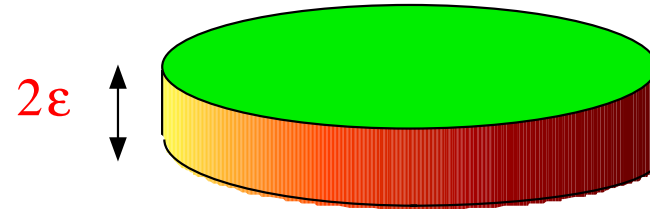
$$\text{div } \sigma = f \quad \text{in } \Omega.$$

Boundary Conditions

Plate $\Omega = \omega \times (-\varepsilon, +\varepsilon)$

with small ε

Mean surface $\omega =$ smooth plane domain.



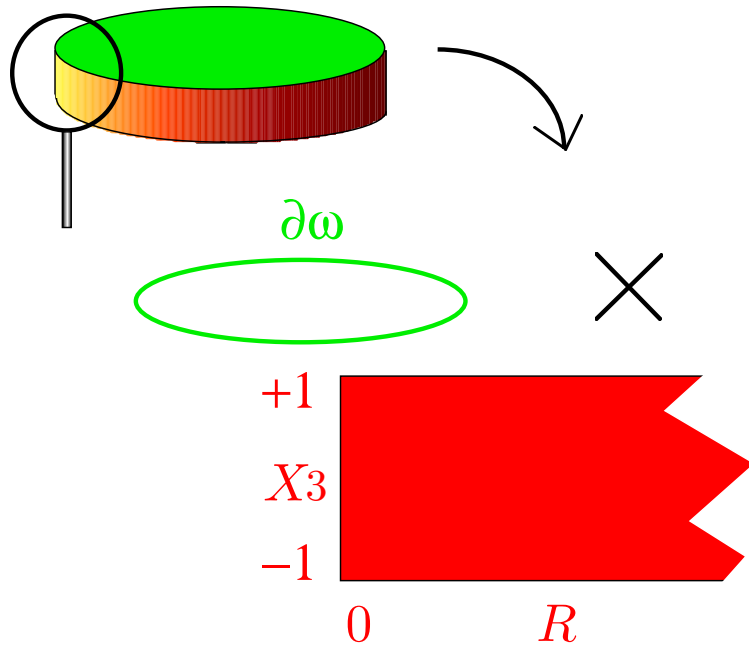
Horizontal boundaries $\omega \times \{\pm\varepsilon\}$

- Zero Traction $T := \sigma(n) = 0$.

Lateral boundary $\partial\omega \times (-\varepsilon, +\varepsilon)$

- ① Hard Clamped $u_s = 0, u_n = 0, u_3 = 0$.
- ② Hard Simple Supported $u_s = 0, T_n = 0, u_3 = 0$.
- ③ Sliding Edge $T_s = 0, u_n = 0, T_3 = 0$.
- ④ Free $T_s = 0, T_n = 0, T_3 = 0$.

Scaled variables



In Ω^ε :

variables $x = (x_1, x_2, x_3)$

In ω :

variables $x_* = (x_1, x_2)$

In ω , near $\partial\omega$:

r distance to $\partial\omega$, s arclength,

$\kappa = \kappa(s)$ curvature.

Scaled vertical variable:

$$X_3 = \frac{x_3}{\varepsilon}$$

Scaled distance to $\partial\omega$:

$$R = \frac{r}{\varepsilon}$$

Membrane answer

Membrane load: $f^\varepsilon(x_*, x_3) = f(x_*, X_3)$, i.e. such that

$$f_\alpha(X_3) = f_\alpha(-X_3) \quad \text{and} \quad f_3(X_3) = -f_3(-X_3)$$

Ingredients

Kirchhoff-Love displacements

$$u_{\text{KL},m}^k(x_*, x_3) = (\zeta_1^k(x_*), \zeta_2^k(x_*), 0)$$

Displacements with mean values zero across each fiber

$$\int_{-1}^{+1} v_m^k(x_*, X_3) dX_3 = 0, \quad \forall x_* \in \omega$$

Boundary layer terms

$$\Phi_m^k(s, R, X_3), \quad \Phi_m^k \text{ exp. decaying as } R \rightarrow \infty$$

Expansion

$$u^\varepsilon \simeq u_{\text{KL},m}^0 + \sum_{k \geq 1} \varepsilon^k \left(u_{\text{KL},m}^k + v_m^k + \Phi_m^k \right)$$

Bending answer

Bending load: $f^\varepsilon(x_*, x_3) = f(x_*, X_3)$, i.e. such that

$$f_\alpha(X_3) = -f_\alpha(-X_3) \quad \text{and} \quad f_3(X_3) = f_3(-X_3)$$

Ingredients

Kirchhoff-Love displacements

$$u_{\text{KL},b}^k(x_*, x_3) = (-x_3 \partial_1 \zeta_3^k(x_*), -x_3 \partial_2 \zeta_3^k(x_*), \zeta_3^k(x_*))$$

Displacements with mean values zero across each fiber

$$\int_{-1}^{+1} v_b^k(x_*, X_3) dX_3 = 0, \quad \forall x_* \in \omega$$

Boundary layer terms

$$\Phi_b^k(s, R, X_3), \quad \Phi_b^k \text{ exp. decaying as } R \rightarrow \infty$$

Expansion

$$u^\varepsilon \simeq \varepsilon^{-2} u_{\text{KL},b}^{-2} + \varepsilon^{-1} u_{\text{KL},b}^{-1} + \sum_{k \geq 0} \varepsilon^k \left(u_{\text{KL},b}^k + v_b^k + \Phi_b^k \right)$$

(Clamped Elliptic Shells – Result by Erwan FAOU)

Loading $f^\varepsilon = f(x_*, X_3)$.

New scale $T = \frac{r}{\sqrt{\varepsilon}}$ (cf Novozhilov & Koiter models) and new profiles

$Z = Z(s, T, X_3)$, exp. decaying as $T \rightarrow \infty$, polynomial in X_3

Expansion

$$u^\varepsilon \simeq u_{\text{KL}}^0 + Z^0 + \sqrt{\varepsilon} \left(u_{\text{KL}}^{\frac{1}{2}} + Z^{\frac{1}{2}} \right) + \sum_{k=1, \frac{3}{2}, 2, \dots} \varepsilon^k \left(u_{\text{KL}}^k + v^k + Z^k + \Phi^k \right)$$

Elastic energy	Membrane Plate	Bending Plate	Elliptic shell
Boundary layer terms	ε^2	ε^0	$\sqrt{\varepsilon}$
In-plane terms	ε	ε^{-1}	ε

Structure of first terms in plates

Displacements with mean values zero — with $p = \frac{\lambda}{6(\lambda+2\mu)}$

$$v_m^1 = p \left(0, 0, -6X_3 \operatorname{div}_* \zeta_*^0 \right) \quad \text{and} \quad v_b^0 = p \left(0, 0, (3X_3^2 - 1) \Delta_* \zeta_3^{-2} \right)$$

Boundary layer profiles (in tensor product form)

$$\Phi_m^1(s, R, X_3) = \ell_m(s) \bar{\Phi}_m(R, X_3) \quad \text{and} \quad \Phi_b^0(s, R, X_3) = \ell_b(s) \bar{\Phi}_b(R, X_3)$$

Case	ℓ_m	$\bar{\Phi}_m$	ℓ_b	$\bar{\Phi}_b$
①	$\operatorname{div}_* \zeta_*^0$	$(0, \bar{\Phi}_n, \bar{\Phi}_3)$	$\Delta_* \zeta_3^{-2}$	$(0, \bar{\Phi}_n, \bar{\Phi}_3)$
②	$\kappa \zeta_n^0$	$(0, \bar{\Phi}_n, \bar{\Phi}_3)$	$\kappa \partial_n \zeta_3^{-2}$	$(0, \bar{\Phi}_n, \bar{\Phi}_3)$
③	0	0	$\kappa \partial_s \zeta_3^{-2}$	$(\bar{\Phi}_s, 0, 0)$
④	0	0	$(\partial_n + \kappa) \partial_s \zeta_3^{-2}$	$(\bar{\Phi}_s, 0, 0)$

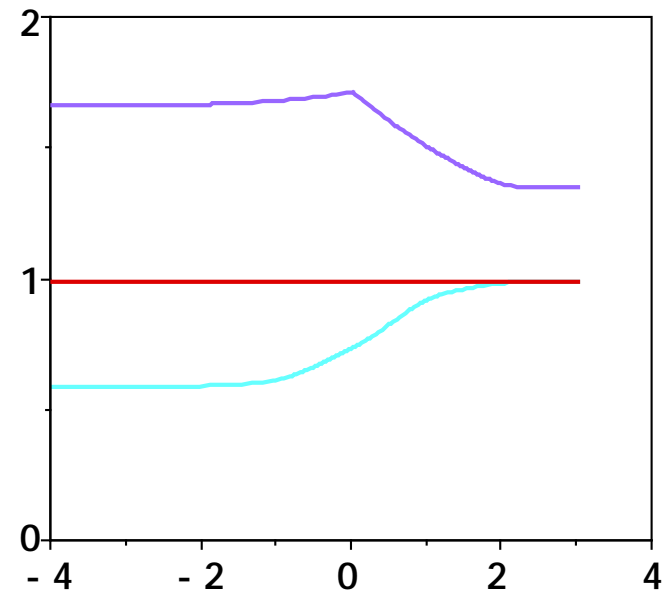
Singularities

The singularities concentrate in the boundary layer terms, via the typical profiles $\bar{\Phi}$.

The $\bar{\Phi}$ have singularities at the corners $(0, \pm 1)$ of the half-strip:

$$\bar{\Phi} = \bar{\Phi}_{\text{reg}}(R, X_3) + \sum_{+,-} \mathcal{S}^{\pm}(\varrho^{\pm}, \vartheta^{\pm})$$

- ① Exponents versus $\log_{10} \frac{\mu}{\lambda}$
Never H^2 .
- ② Singularity in $\varrho \log \varrho$. Almost H^2 .
- ③ Singularity in $\varrho^2 \log \varrho$. Almost H^3 .
- ④ Idem.



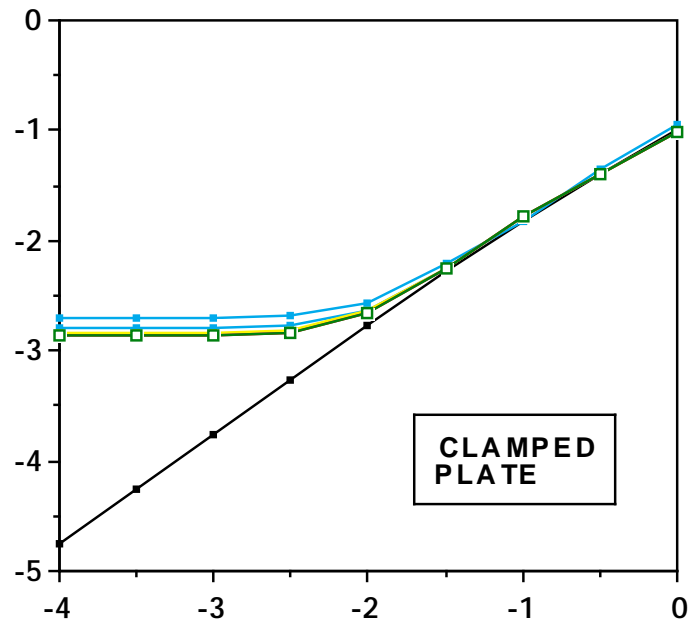
— First exponent
— Second exponent

Boundary layers in Strains

In order to measure boundary layer effects we introduce the quantity

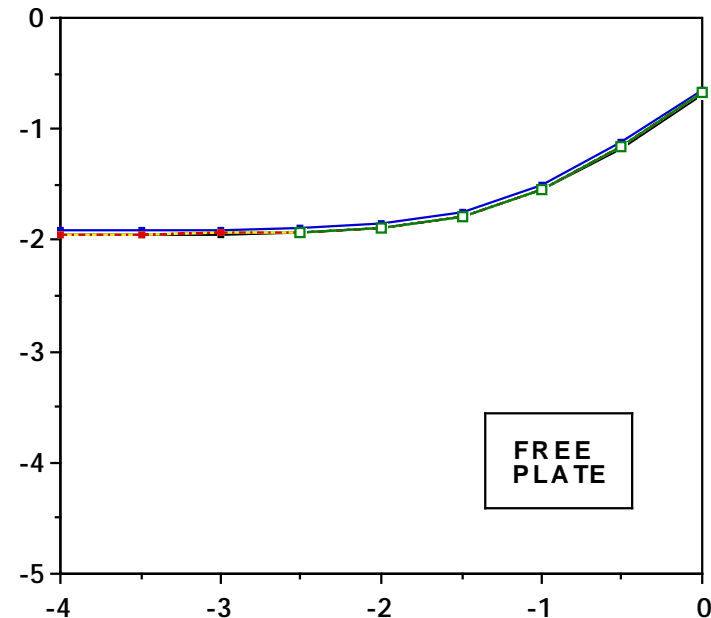
$$I_{ij} = \left(\frac{1}{V} \int_{s=s_1}^{s_2} \int_{r=0}^{\epsilon} \int_{x_3=-\epsilon}^{\epsilon} |e_{ij}|^2 dV \right)^{\frac{1}{2}}$$

Clamped plate: $e_{r3} = e_{RX_3}[\Phi^1] + \epsilon(\dots)$. **Free plate:** $e_{s3} = e_{sX_3}[\Phi^1] + \epsilon(\dots)$.



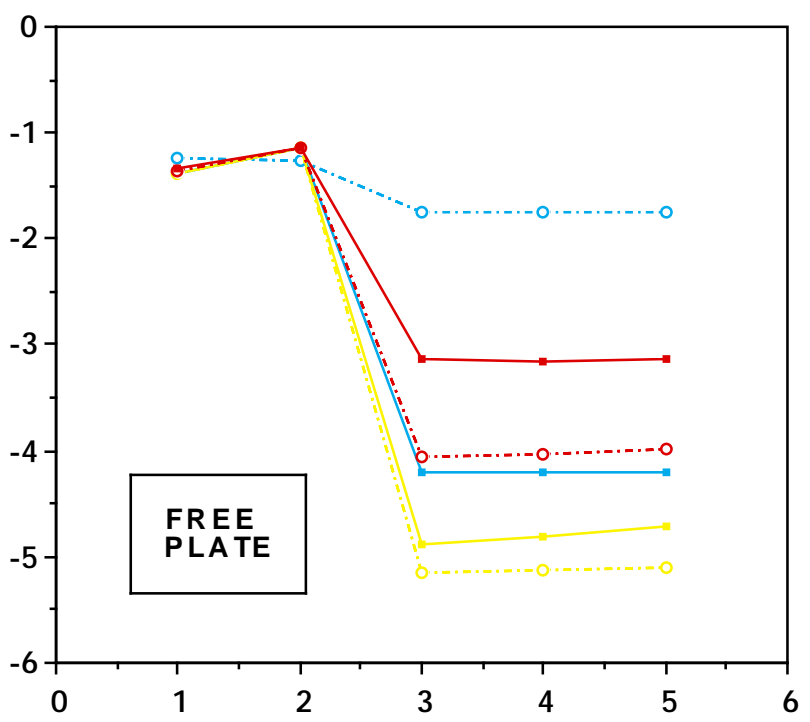
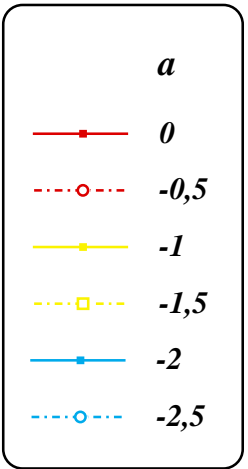
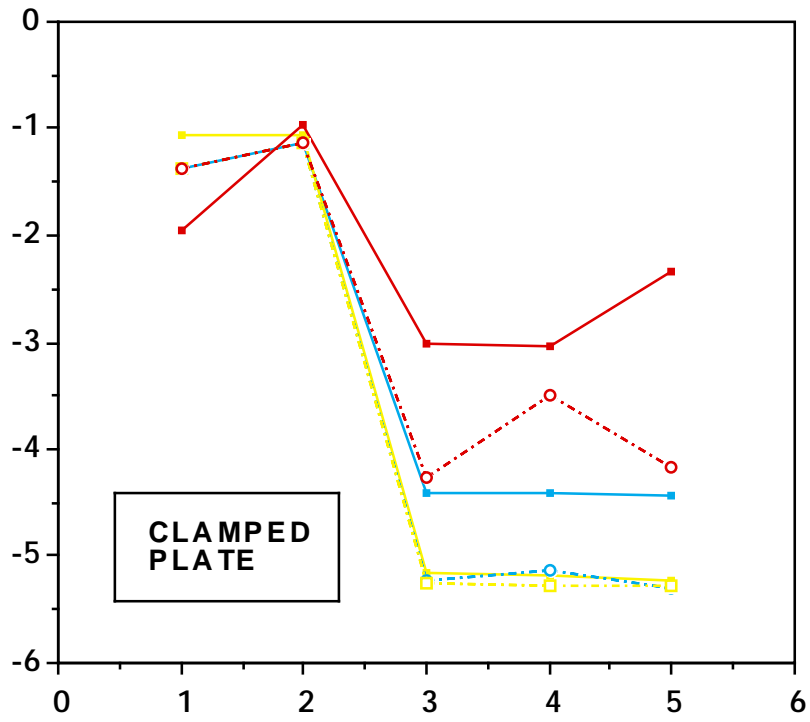
$\log_{10} I_{r3}$ versus $\log_{10} \epsilon$.

With different models.



$\log_{10} I_{s3}$ versus $\log_{10} \epsilon$.

Convergence of models outside the boundary layer

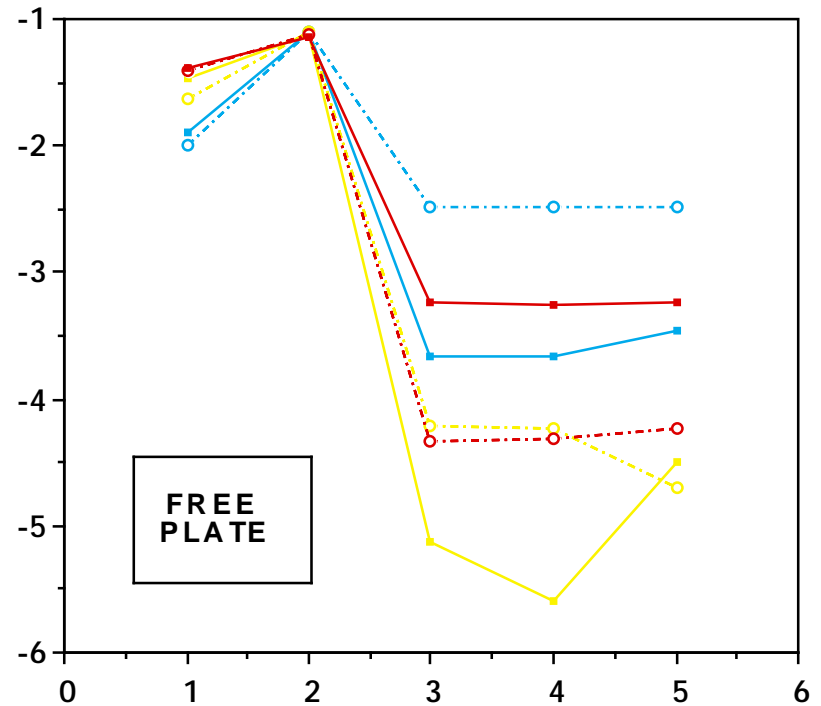
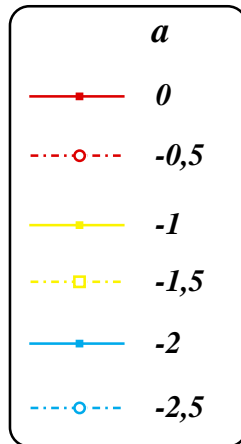
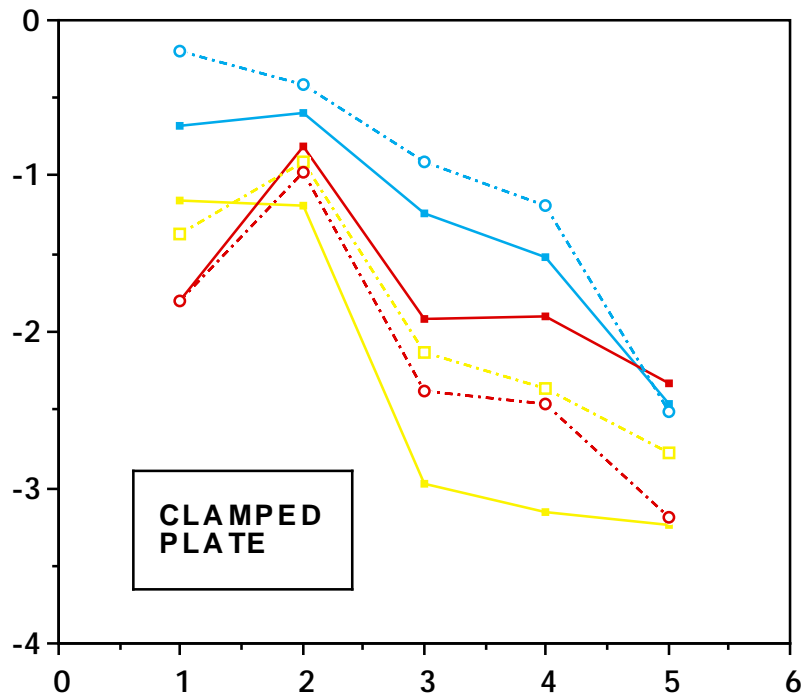


Abscissa : the degree in the hierarchy
Ordinates : \log_{10} of the relative error with 3D.
 Each curve : a value of $\epsilon = 10^a$.

Degree	1	2	3	4	5
In-plane	1	1	3	3	5
Tranverse	0	2	2	4	4



Convergence of models inside the boundary layer



Abscissa : the degree in the hierarchy (in StressCheck)

Ordinates : \log_{10} of the relative error with 3D. Different ranges for clamped and free.

Each curve : a value of $\epsilon = 10^a$.

Prospects

- **Shallow shells**, general material law with non-necessarily clamped boundary conditions: in progress with **Georgiana ANDREOIU** and **Erwan FAOU**.
- **Modal analysis** for lowest families of eigenvalues in thin structures: in progress with **Ivica DJURDJEVIC**, **Erwan FAOU** and **Andreas RÖSSLE**.
- Modal analysis for **High frequencies** in thin structures: planned with **Sergei NAZAROV** and **Andreas RÖSSLE**.
- **Shells**: in progress by **Erwan FAOU**.
- **Plates with corners**: planned with **Martin COSTABEL** and **Andreas RÖSSLE**.
- **Numerical experiments** with **Zohar YOSIBASH**.