

Reactive Transport

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Objective

- Motivate the need for Reactive transport
- Present a methodology to do it

CONTENTS

- Background
 - Framing reactive transport
 - Types of problems: is it needed?
 - A bit of chemistry
- General approach
- Examples
- What about heterogeneity?

Porous media ... and we are just starting...



Summary (things you need to know)

Reactive transport requires **two ingredients** 1) Transport (advection, dispersion, mixing, and all that)

- 2) Reactions: many types, complex (you need to work with someone who knows the types of reactions we are going to work with), but conceptually easy
- 3) We need appropriate nomenclature to work with these things (a table is a flat surface on which you can eat... or work... with 3 or four legs that separate it from the soil...)

But, aren't there many reactions?

Indeed!

The technology of geochemistry is complex but not conceptually difficult

Ingredient 1: solute transport

- Advection: $\mathbf{v} = \mathbf{q}/\phi$ (q proportional to K)
- Dispersion: Proportional to: αq
- Reactions
- Mass Conservation

$$\phi \frac{\partial c}{\partial t} = \nabla (\mathbf{D} \nabla c) - \mathbf{q} \nabla c + f - r$$
Porosity
Dispersion
Coeff.
Water
Reactions

Written compactly $\mathcal{L}(\mathcal{C}) = -\mathbf{q} \cdot \nabla \mathcal{C} + \nabla \cdot (\mathbf{D} \nabla \mathcal{C})$

To simplify chemistry, let us introduce matrix notation ...even better, vector space notation

• Traditional notation
-
$$HCO_3^- \rightarrow H^+ + CO_3^{2-}$$

- $H_2CO_3 \rightarrow 2H^+ + CO_3^{2-}$
• Matrix notation
 $\mathbf{S}_{\mathbf{e}} \log \mathbf{a} = \log \mathbf{K}$
 $\begin{pmatrix} 1 & 1 & -1 & 0 \\ 2 & 1 & 0 & -1 \end{pmatrix} \begin{pmatrix} \log a_{H^+} \\ \log a_{CO_3^-} \\ \log a_{HCO_3} \\ \log a_{HCO_3} \\ \log a_{H_2CO_3} \end{pmatrix} = \begin{pmatrix} \log K_1 \\ \log K_2 \end{pmatrix}$

Ingredient 2: Chemical reactions: Stoichiometric matrix

Assume a chemical system

 $\mathcal{CO}_3^{2-} = \mathcal{HCO}_3^{-} - \mathcal{H}^+$ $\mathcal{CO}_2 = \mathcal{HCO}_3^- + \mathcal{H}^+ - \mathcal{H}_2\mathcal{O}$ $\mathcal{C}a^{2+} = \mathcal{C}a\mathcal{C}O_{3s} + \mathcal{H}^{+} - \mathcal{H}\mathcal{C}O_{3}^{-}$

Let r_i be the number of moles of reactants that evolve into products for the i-th reaction

• Stoichiometric Matrix (rows: reactions; columns: species)



each species

Reaction rate: Mass balance • $R = S^{\dagger}r$

Contribution of reactions to the mass balance of each species

Reactive transport

Reactions

 $r_1 CO_3^{2-} = HCO_3^{-}(-H^+)$ $r_2 CO_2 = HCO_3 + H^+ + H_2O$ $r_3 Ca^{2+} = CaCO_3 + H^+ - HCO_2^-$

Let r_i be the number of moles of reactants that evolve into products for the i-th reaction

- Transport of all species
- $\phi \frac{\partial \mathcal{H}^{+}}{\partial t} = \mathcal{L}(\mathcal{H}^{+}) r_{1} + r_{2} + r_{3} \qquad \phi \frac{\partial \mathcal{HCO}_{3}^{-}}{\partial t} = \mathcal{L}(\mathcal{HCO}_{3}^{-}) + r_{1} + r_{2} r_{3}$ $\phi \frac{\partial \mathcal{CO}_{3}^{2-}}{\partial t} = \mathcal{L}(\mathcal{CO}_{3}^{2-}) - r_{1} \qquad \phi \frac{\partial \mathcal{CO}_{2}}{\partial t} = \mathcal{L}(\mathcal{CO}_{2}) - r_{2} \qquad \phi \frac{\partial \mathcal{Ca}^{2+}}{\partial t} = \mathcal{L}(\mathcal{Ca}^{2+}) - r_{3}$ Recall S
 - $\mathbf{S} = \begin{pmatrix} \mathcal{H}^+ & \mathcal{HCO}_3^- & \mathcal{CO}_3^{2-} & \mathcal{CO}_2 & \mathcal{Ca}^{2+} & \mathcal{CaCO}_{3s} & \mathcal{H}_2\mathcal{O} \\ \hline 1 & 1 & -1 & 0 & 0 & 0 \\ \hline 1 & -1 & 0 & -1 & 0 & 0 & -1 \\ \hline 1 & -1 & 0 & 0 & -1 & 1 & 0 \end{pmatrix}$ Primary Secondary Constant Ac.

$$\frac{\partial \mathbf{c}}{\partial t} = \mathbf{M} \mathcal{L}(\mathbf{c}) + \mathbf{S}_{e}^{\dagger} \mathbf{r}_{e} + \mathbf{S}_{k}^{\dagger} \mathbf{r}_{k}(\mathbf{c}) \quad n_{s} \text{ transport equations}$$

$$S_{ea} \log c_a = \log K$$

$$r_k = r_k(c)$$

$$n_r \text{ algebraic equations}$$

Looks awful! $(n_r + n_s \text{ unknowns at every point})$

Seek tricks and/or simplifications

And, thus, insight

So... objectives of this presentation

- Is reactive transport needed?
 - Wouldn't it be sufficient to find the residence time distribution to find out the total amount of reactions?
- Can be understood?
- Can be solved efficiently?
 - ... and the answer is YES
- Do we really know how to do it? ... not quite... but getting there ... hopefully

Why worry about reactive transport? Ex: Karst development in coastal areas



Calcite dissolution in coastal aqf.

Mixture of two calcite saturated waters may be under or oversaturated with respect to calcite



Salinity

To simulate this effect, consider 1D diffusion experiment freshwater calcite saltwater

Saturation Index



SI & r



Speciation



Dissolution causes diffusion of CO_2 (acidity) at the freshwater end, which drives further dissolution

Sensitivity to CO_2



Reducing concentration of CO_2 at the freshwater end, causes an increase in subsaturation. Therefore, one would expect an increase in dissolution rate

However, dissolution rate is dramatically reduced

First conclusion

The interplay between transport and reactions is non-trivial.

- Saturation index calculations are needed but they fail to indicate
- 1) how much calcite is dissolved, which is controlled by mixing rate,
- 2) nor where (or under which conditions) dissolution rate is maximum.

Simulating reactive transport is needed to understand the fate of reacting solutes!

(Rezaei et al, 2005)

Still, isn't it too difficult?

- Yes, if using brute force
- However, a number of "tricks" are possible, depending on the type of chemical system
 - If all reactions in equilibrium (Desimoni et al, 2005)
 - If also kinetic reactions (Molins et al, 2007)
 - In general (Saaltink et al, 1998)

The basic trick: components

$$\frac{\partial \mathbf{c}}{\partial t} = \mathbf{M} \mathcal{L}(\mathbf{c}) + \mathbf{S}_{e}^{t} \mathbf{r}_{e} + \mathbf{S}_{k}^{t} \mathbf{r}_{k}(\mathbf{c})$$

Choose component matrix U, such that

$$\mathsf{US}_{e}^{\dagger}=0 \Rightarrow \mathsf{US}_{e}^{\dagger}\mathsf{r}_{e}=0$$

Then,

$$\mathbf{U}\frac{\partial \mathbf{c}}{\partial t} = \mathbf{U}\mathbf{M}\mathcal{L}(\mathbf{c}) + \mathbf{U}\mathbf{S}_{\mathbf{k}}^{\dagger}\mathbf{r}_{\mathbf{k}}(\mathbf{c})$$

Components: $\mathbf{u} = \mathbf{U}\mathbf{c}$

Linear combinations of species that remain unaltered by equilibrium reactions

 $n_s - n_r$ transport equations.

(A good choice of U allows to decouple (some of) these equations!)

Example

- Chemical system $CO_3^{2-} = HCO_3^{-} H^+$ $CO_2 = HCO_3^{-} + H^+ - H_2O$ $Ca^{2+} = CaCO_{3s} + H^+ - HCO_3^{-}$
- Stoichiometric Matrix $S_e = (S_1; -I)$ $S_e = \begin{pmatrix} H^+ & HCO_3^- & CO_3^{2-} & CO_2 & Ca^{2+} \\ -1 & 1 & -1 & 0 & 0 \\ 1 & 1 & 0 & -1 & 0 \\ 1 & -1 & 0 & 0 & -1 \end{pmatrix}$
- Components matrix $U=(I; S_1^+)$ $U = \begin{pmatrix} H^+ & HCO_3^- & CO_2 & Ca^{2+} \\ 1 & 0 & -1 & 1 & 1 \\ 0 & 1 & 1 & 1 & -1 \end{pmatrix}$
- Components
 - $u_{1} = H^{+} CO_{3}^{2-} + CO_{2} + Ca^{2+} \text{ (acidity)}$ $u_{2} = HCO_{3}^{-} + CO_{3}^{2-} + CO_{2} - Ca^{2+} \text{ (Total Inorganic Carbon)}$

Role of components

$$\phi \frac{\partial \mathcal{H}^{+}}{\partial t} = \mathcal{L}(\mathcal{H}^{+}) - r_{1} + r_{2} + r_{3}$$

$$\phi \frac{\partial \mathcal{H}CO_{3}^{-}}{\partial t} = \mathcal{L}(\mathcal{H}CO_{3}^{-}) + r_{1} + r_{2} - r_{3}$$

$$\phi \frac{\partial \mathcal{C}O_{3}^{2-}}{\partial t} = \mathcal{L}(\mathcal{C}O_{3}^{2-}) - r_{1}$$

$$\phi \frac{\partial \mathcal{C}O_{2}}{\partial t} = \mathcal{L}(\mathcal{C}O_{2}) - r_{2}$$

$$\phi \frac{\partial \mathcal{C}a^{2+}}{\partial t} = \mathcal{L}(\mathcal{C}a^{2+}) - r_{3}$$

$$u_{1} = \mathcal{H}^{+} - \mathcal{C}O_{3}^{2-} + \mathcal{C}O_{2} + \mathcal{C}a^{2+}$$

$$u_{2} = \mathcal{H}CO_{3}^{-} + \mathcal{C}O_{3}^{2-} + \mathcal{C}O_{2} - \mathcal{C}a^{2+}$$

 $\mathbf{U} = \begin{pmatrix} \mathcal{H}^{+} & \mathcal{HCO}_{3}^{-} & \mathcal{CO}_{3}^{2-} & \mathcal{CO}_{2} & \mathcal{Ca}^{2+} \\ 1 & 0 & -1 & 1 & 1 \\ 0 & 1 & 1 & 1 & -1 \end{pmatrix}$

Components are linear combinations of species such that equilibrium r's cancel out, so that $\phi \frac{\partial u_1}{\partial t} = \mathcal{L}(u_1)$

Procedure

- 1. Define chemical system and components
- 2. Solve transport equations for components (and/or primary species)
- **3.** Speciation: Compute species concentrations from components (and/or primary species)
- 4. Substitute species back into transport equations to obtain reaction rates

Analytical solution for 2 species

Assume 2 species (e.g. SO_4^{2-} and Ca^{2+}) in eq. with gypsum Step 1: Chemical system Reaction $Ca^{2+} + SO_4^{2-}$ $CaSO_{4s} \Rightarrow \lceil Ca^{2+} \rceil \cdot \lceil SO_4^{2-} \rceil = K$ Stoichiometric matrix $S_e = (-1 \ -1 \ 1)$ Components: $U = (1 - 1) \Rightarrow u = \lceil Ca^{2+} \rceil - \lceil SO_4^{2-} \rceil$ is conservative! Step 2: Solve transport of u Transport equations $\frac{\partial (\phi C_1)}{\partial t} - \mathcal{L}(C_1) = -r \quad (1)$ $\frac{\partial (\phi C_2)}{\partial t} - \mathcal{L}(C_2) = -r \quad (2)$ where $\mathcal{L}(c) = -\mathbf{q} \cdot \nabla c + \nabla \cdot (\mathbf{D} \nabla c)$ (1)-(2) yields: $\frac{\partial(\phi u)}{\partial t} = \mathcal{L}(u)$

Analytical solution for 2 species



Step 4: Compute r Plugging C_2 into $\frac{\partial(\phi C_2)}{\partial t} - \mathcal{L}(C_2) = -r$ $\mathcal{L}(c) = -\mathbf{q} \cdot \nabla c + \nabla \cdot (\mathbf{D} \nabla c)$ Transport We obtain $r = \frac{\partial^2 C_2}{\partial u^2} [\nabla u^T \cdot \mathbf{D} \cdot \nabla u]$ Chemistry $\frac{\partial^2 C_2}{\partial u^2} = \frac{2K}{(u^2 + 4K)^{3/2}}$

Mixing of several waters

Step 3: Speciation

Can be very complex, but $C_2 = C_2(\alpha)$

Where α is the mixing ratio (possibly a vector)

Step 4: Compute r Plugging C_2 into $\frac{\partial(\phi C_2)}{\partial t} - L_t(C_2) = -$ That is, We obtain $r = \frac{\partial^2 C_2}{\partial \alpha^2} [\nabla \alpha^T \cdot \mathbf{D} \cdot \nabla \alpha]$ 1) Transport α 2) Use any code (e.g., PHREEQE, RETRASO,...) to compute speciation

Mixing rate controls (fast) reactions

- Mixing controls fast chemical reactions (de Simoni et al, 2005, 2007; Valocchi & Cirpka, 2007)
- In fact, reaction rate of equilibrium reactions $r = \mathbf{H} \nabla^T c \cdot \mathbf{D} \cdot \nabla c = f_Q \cdot f_m$
- Natural choice for (local) mixing rate $f_m = \nabla^T c \cdot \mathbf{D} \cdot \nabla c$

(de Simoni et al, 2005, 2007; Kitanidis, 1994)

2nd Conclusion

In the case of aqueous and dissolutionprecipitation reactions in equilibrium:

- 1. Reactive Transport is indeed easy!
- Only need to solve for independent components. In the calcite example:2 components are needed (+salinity)... Actually, it suffices to work with mixing ratios... (Desimoni et al., 2007). And, now, not even that (just mixing rates!)
- 3. Mixing drives fast reactions

Does it work?



But do we know how to represent mixing? Does dispersion represent mixing?

Dispersion = the rate of growth of plumes

Therefore Dispersion=spreading rate

$$D = \frac{1}{2} \frac{\partial \sigma_{ii}^2}{\partial t}$$

Mixing reflects local gradients (internal disorder within a plume)



Non-local (in t) formulations for RT



Non-local (in t) formulations for RT

Willmann et al (WRR, 2010) predicted quite accurately the overall (integrated in t and z) reaction rate, and thus mixing using a MRMT formulation



Non-local formulations reproduce mixing, but Willman required a tracer test to characterize memory function, can it be defined from site characterization?

Conclusion 2

- Non-local formulations reproduce
- Scale dependence of dispersion (spreading)
- Scale dependence of apparent porosity
- Tailing
- -Not too bad for reaction rates (mixing)
- and easy to implement in existing codes!
- Mixing is the critical issue, but:
- Can mixing be defined from geological characterization?
- -Is it true that mixing well represented by MRMT?

OBJECTIVE

- Test validity of MRMT
 - First, separate mixing from spreading
 - Second, select right memory fuction

Numerical simulations of mixing in <u>heterogeneous porous media</u>

150

300

250

adad.

150

Add



- Multi-lognormal permeability fields
- Log permeability field variance s² InK
- Gaussian correlation function
- Correlation length λ =10
- Permeater boundary conditions
- Steady flow

- Initial line injection
- Domain size 512x8192
- Local advection-diffusion

scale log_{to}K and log

• Peclet number:

$$Pe = \frac{\lambda \overline{v \nabla h}}{D} = 10^2 - 10^3$$



Global mixing and spreading



Use dissipation rate to compute overall mixing

Separate mixing rate (and state) into macrodispersion driven (reference) and internal disorder driven

Separating mixing and spreading?

1. Decompose c:

$$c = \overline{c} + c'$$

2. Vertical averaging

$$\overline{c}(x,t) = \frac{1}{Ly} \int_{0}^{Ly} c(x,y,t) dy$$

3. Compute variance of averaged concentration (reference mixing state, controlled by macrodispersion)

$$\mathcal{M}_{1}(t) = \int_{0}^{L_{x}} \overline{c}^{2} dx \quad \mathcal{M}_{\mathcal{G}} = \frac{m_{0}^{2}}{2L_{2}\sqrt{\pi}\sigma_{L}}$$

4. Compute "internal mixing" (caused by internal disorder):

$$\mathcal{M}_{2}(t) = \int_{\Omega} (c')^{2} dV$$

Separating mixing and spreading?

$$\mathcal{M}_{1}(t) = \int_{0}^{L_{x}} \overline{c}^{2} dx \quad \mathcal{M}_{\mathcal{G}} = \frac{m_{0}^{2}}{2L_{2}\sqrt{\pi}\sigma_{L}}$$

$$\mathcal{M}_{2}(t) = \int_{\Omega} (c')^{2} dV$$

1. Clearly:
$$M(t) = \int_{\Omega} c^2 dx \quad M_{\mathcal{G}} + M_2$$

2. Therefore, it is natural to measure "internal disorder" by:

$$\gamma(t) = \frac{M_2(t)}{M_G(t)} = \frac{M(t) - M_G(t)}{M_G(t)}$$

Characterizing the γ function

Mixing and spreading identical at late times (even though not fully mixed)

†=1

t=3.3

t=9.3

t=24

Variance of c'

(De Dreuzy et al., WRR, 2012)

Characterizing γ max and tmax

MRMT formulations do reproduce the shape of gamma

But not the actual values!

£X/v

Summary and conclusions

- Spreading can be described by the pdf and transition pdf of veloc, which leads to CTRW, MRMT, fADE,...
- These formulations overcome the ADE problems, but rely heavily on a proper characterization of mixing.
- We developed methodology for effective mixing that relies on the evolution of the variance of c'.
- Non local equations parameters (memory function) look valid, but not quite.

Any idea?

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Redox reactions involve exchange of electrons (e⁻) The species giving electrons away is called "electron donor", the one receiving is the "electron acceptor", eg. $Fe^{2+} \rightarrow Fe^{3+} + e^{-}$ O_2 + 4H⁺ + 4e⁻ \rightarrow 2H₂O $4 \text{ Fe}^{2+} + \text{O}_2 + 4\text{H}^+ \rightarrow 4\text{Fe}^{3+} + 2\text{H}_2\text{O}$ Iron is donor (is oxidized). Oygen is acceptor (is reduced) These reactions are exothermic. Life on Earth is sustained on the energy freed by these reactions.

Biochemical reactions: the natural redox cycle

- Redox reactions catalyzed by microorganisms
- Special case: organic matter **degradation**, the electron donor is organic matter (generically, CH_2O). The **natural sequence** is:
 - $CH_2O + O_2 \rightarrow CO_2 + H_2O$ $\Delta G=120 \text{ kcal/mol } C$
 - $CH_2O + 0.8NO_3^- + 0.8H^+ \rightarrow CO_2 + 0.4N_2 + 1.4H_2O$ $\Delta G=114$
 - $CH_2O + 2MnO_2 + 4H^+ \rightarrow CO_2 + 2Mn^{2+} + 3H_2O$ $\Delta G=81$
 - $CH_2O + 4Fe(OH)_3 + 8H^+ \rightarrow CO_2 + 4Fe^{2+} + 11H_2O$ $\Delta G=28$
 - $CH_2O + 0.55O_4^{2-} + H^+ \rightarrow CO_2 + 0.5H_2S + H_2O$ $\Delta G=25$
 - CH_2O (0.5 CH_2O +0.5 CH_2O)→ 0.5 CO_2 + 0.5 CH_4 $\Delta G=22$

The most **efficient organisms dominate each stage**, inhibiting the development of the ones below. Yet, their success is their nemesis, as they **exhaust their electron acceptor**. This opens the path for the **next organism down the ladder**, which dominates the next stage. Overall, this leads to a **natural zonation**.

Why biological degradation

- Control metal mobility
 - Many immobile when sulphide present
 - Some immobile in aerobic conditions
- Control degradation of organic matter
- Highly reducing conditions allow eliminating "recalcitrant" compounds
 - That are not eliminated in "normal" treatment
 - That are often endocrine inhibitors

Redox zones at the Vejen (Denmark) landfill

Conclusions

- Is Reactive transport needed?
 - Reaction (rate , where, when, under which conditions) are controlled by transport.
- Can be understood?
 - All it takes is to understand components
 - The difficult part is to choose the relevant species and reactions.
- Can be solved efficiently?
 - Similar effort as conservative transport

Reactions are driven by **disequilibrium**

Disequilibrium is driven by actual mixing

We need to know how to evaluate actual mixing!

Current stochastic transport theories fail to do so!

